

Dependence on the Armchair/Zigzag Edge Ratio of the Melting Process of Armchair Hexagonal Boron Nitride Nanoribbon

Hang T. T. Nguyen^{1,2,*}



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ABSTRACT

The dependence of the melting point on the armchair/zigzag (A/Z) edge ratios in armchair hexagonal boron nitride nanoribbons (h-BNNR) is investigated through molecular dynamics simulations. For this purpose, initial configurations with eight different A/Z edge ratios (0.017377, 0.069510, 0.278481, 0.434782, 1.724409, 6.968254, 10.745098, and 43.88) of armchair h-BNNRs, each containing the same number of atoms (10,000 identical B and N atoms), are heated from 50 K to 7000 K using the Tersoff potential. The initial (0.017377 A/Z ratio) and the final (43.88 A/Z ratio) configurations significantly influence the melting process of the armchair h-BNNRs: The 0.017377 A/Z configuration exhibits a high melting point (5300 K) compared to the subsequent seven cases; the melting process in the 43.88 A/Z ratio configuration is markedly influenced by finite size effects. The melting points of the intervening six configurations are relatively unaffected by the A/Z edge ratio, with an average melting point of 4180 K for these configurations. When analyzing a system with 10,000 atoms, the critical A/Z edge ratio is identified at 10.745098. At this critical A/Z edge ratio, the melting point shows minor fluctuations around 4040 K when the number of atoms in the configuration is increased from 10,000 to 25,600 atoms. It is noted that, at this critical A/Z ratio, the melting point is not significantly affected by an increase in the number of atoms within the configuration.

Key words: Melting of armchair hexagonal boron nitride nanoribbon, A/Z edge ratio dependence, Critical armchair/zigzag edge ratio, Finite size effects

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1 INTRODUCTION

2 The remarkable properties of two-dimensional materials have garnered considerable attention in recent 3 years, owing to their unique electronic, thermal, and 4 mechanical characteristics. Graphene, a single layer 5 of carbon atoms arranged in a hexagonal lattice, has 6 emerged as a revolutionary material with extraordinary 7 properties, revolutionizing the landscape of materials 8 science and technology¹. Beyond graphene, 9 a rich family of two-dimensional materials, often referred 10 to as "graphene-like" materials, has been discovered, 11 each with its own unique characteristics and applications. 12 Materials such as hexagonal boron nitride (h-BN)²⁻⁵, 13 transition metal dichalcogenides^{6,7}, and black phosphorus 14 (phosphorene)^{8,9} are among the graphene-like materials 15 that have garnered attention for their unique properties. 16 h-BN, for instance, is an insulator with excellent thermal 17 stability, serving as an ideal substrate for graphene-based 18 devices^{5,10-13}. Armchair hexagonal boron nitride 19 nanoribbons (h-BNNR) are narrow strips of h-BN 20 with specific edge configurations that can be tailored 21 to exhibit distinct electronic behaviors¹⁴⁻¹⁶. Therefore, 22 armchair h-BNNR stands out as a promising 23 candidate due to its intriguing combination of properties. 24

candidate due to its intriguing combination of properties.

The thermal properties of armchair h-BNNR are not only of fundamental interest but also hold significant practical implications for nanoelectronics¹⁷, thermal management¹⁸, and materials science. As the width of these nanoribbons is reduced towards the nanoscale, quantum size effects become increasingly pronounced, resulting in unique thermal behaviors^{19,20}. Additionally, the specific edge configurations, whether zigzag or armchair, can have a profound impact on their thermal properties^{11,21,22}. This influence stems from the altered phonon dynamics, lattice vibrations, and thermal transport mechanisms at the edges of the ribbons.

Up to now, the implementation of the armchair h-BN melting process has encountered many challenges. However, experimental results have been obtained for h-BN in powder form. Powder h-BN has a high melting point, typically around 3000°C (depending on the purity and crystalline structure)²³. This high melting point is due to the strong covalent bonds between boron and nitrogen atoms, similar to those in diamond and graphite in carbon-based materials.

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49 Understanding the interplay between size, edge struc-
 50 ture, and thermal behavior in armchair h-BNNR
 51 is not only essential for fundamental insights into
 52 nanoscale heat transport but also holds the potential
 53 for the design of advanced nanomaterials with tai-
 54 lored thermal characteristics for diverse technologi-
 55 cal applications. In this study, by using molecular dy-
 56 namics (MD) simulation, we delve into the depen-
 57 dence of the melting process of armchair h-BNNR on
 58 the armchair/zigzag (A/Z) ratio and define the critical
 59 A/Z ratio. Note that the melting point of the configu-
 60 ration having this critical A/Z ratio will not be signifi-
 61 cantly affected when the number of atoms in the con-
 62 figuration is increased. Details on the calculation are
 63 given in Section 2. Results and discussion are shown
 64 in Section 3. Conclusions are presented in the last sec-
 65 tion of the paper.

66 **CALCULATION**

67 One of the critical aspects of MD simulations is the
 68 choice of interatomic potential functions, which gov-
 69 ern the interactions between particles in the simulated
 70 system. Among these potential functions, the Tersoff
 71 potential stands out as a versatile and widely used
 72 model, particularly in the study of covalent and semi-
 73 covalent materials. Unlike simple pairwise poten-
 74 tials like Lennard-Jones, the Tersoff potential offers
 75 a more sophisticated description of bond-breaking
 76 and bond-forming events, capturing the intricacies of
 77 chemical bonding and the structural changes that oc-
 78 cur during the simulation.

79 This potential model is particularly adept at reproduc-
 80 ing key material properties, including the prediction
 81 of lattice constants, elastic constants, phonon spectra,
 82 and defect energetics. Moreover, it excels in simu-
 83 lating complex phenomena like dislocations, chemi-
 84 cal reactions, and the mechanical behavior of materi-
 85 als under extreme conditions. The Tersoff potential's
 86 flexibility and versatility stem from its parametriza-
 87 tion, which allows researchers to tailor the potential
 88 parameters to specific materials and applications.
 89 In this study, the interactions between and in the
 90 initial configurations are described by Tersoff poten-
 91 tial²⁴ which is written as below:

$$E_b = \frac{1}{2} \sum_{i \neq j} f_c(r_{ij}) [f_R(r_{ij}) + b_{ij} f_a(r_{ij})]. \quad (1)$$

92 Here, r_{ij} is the distance from atom i to atom j . The
 93 repulsive $f_R(r_{ij})$ and the attractive $f_a(r_{ij})$ terms are
 94 based on Morse potential as proposed by Brenner²⁵.
 95 The cutoff function using for calculating the number
 96 of neighbors as well as making the potential to zero
 97 outside the interaction shell is $f_c(r_{ij})$ term.

We use the software package Large-Scale 98
 Atomic/Molecular Massively Parallel Simulator 99
 to perform the MD simulation²⁶. The ISAACS 100
 software is used to calculate some thermal quan- 101
 tities²⁷. To visualize the atomic configuration, we 102
 use VMD software²⁸. The temperature increase as: 103
 $T = T_0 + \gamma t$, in which, $T_0 = 50\text{K}$ is the initial value of 104
 temperature of the simulation, γ is a heating rate, and t 105
 is the time required for heating. Note that, the heating 106
 rate in this study is 10^{12} K/s. To study the structural 107
 characteristics at given temperatures, configurations 108
 are relaxed for 6×10^5 MD steps (0.0001 picoseconds 109
 per step) to ensure the configuration stability. 110

To study the dependence on the A/Z edge ratio of h- 111
 BNNR melting process, all initial armchair h-BNNR 112
 configurations have to be the same number of atoms 113
 (10,000 atoms) but differ in zigzag- and armchair- 114
 edge lengths. To keep the number of atoms of the 115
 initial configurations being 10,000 atoms, we have to 116
 adjust the length of the armchair and zigzag edges as 117
 shown in Table 1. 118

The simulation passes some stages below: 119

- i) To ensure the configuration stability, the initial con- 120
 figurations are relaxed for MD steps at 50 K under peri- 121
 odic boundary conditions using canonical ensemble 122
 simulation 123
- ii) To have armchair h-BNNR, non-periodic bound- 124
 ary conditions with an elastic reflection behavior are 125
 applied along the zigzag edges after adding a space of 126
 20 \AA at both ends. After that, initial configuration are 127
 relaxed again to equilibrium further for MD steps at 128
 50 K using canonical ensemble simulation 129
- iii) The configurations are heated up to about 7000 130
 K which is higher than the melting point of zigzag 131
 h-BNNR¹¹ to ensure that at the chosen temperature 132
 (7000 K) all configurations are in a liquid state. 133

134 **RESULTS AND DISCUSSION**

To study the thermodynamic properties of materials 135
 upon heating, the total energy per atom plays a crucial 136
 role which helps in understanding how a material 137
 responds to changes in temperature. Based on the total 138
 energy per atom one can observe the phase transi- 139
 tions and the temperature at the phase transitions 140
 such as melting point. In this study, to investigate the 141
 influence of armchair and zigzag edges on the melt- 142
 ing process of armchair h-BNNR the total energy per 143
 atom of eight configurations in Table 1 is calculated 144
 and presented in Figure 1. 145

Based on the results of the total energy per atom 146
 (square symbol in Figure 1) one can see that except 147
 for Configuration 8 in Table 1 (square symbol in Fig- 148
 ure 1 h), the graphs of the total energy per atom of the 149

Table 1: The zigzag- and armchair-edge lengths of the armchair h-BNRR.

Configurati	1	2	3	4	5	6	7	8
Length (Å)								
Zigzag-edge	22	44	88	110	219	439	548	1097
Armchair-edge	1266	633	316	253	127	63	51	25
A/Z ratio	0.017377	0.069510	0.278481	0.434782	1.724409	6.968254	10.745098	43.88

150 other configurations in Table 1 (square symbol in Fig-
 151 ure 1 a-g) divide into two regions: i) In the first region,
 152 the graph of the total energy per atom for each con-
 153 figuration increases linearly to a certain value of tem-
 154 perature. This indicates that the configurations are in
 155 a crystal state. At this state, the atoms in the configu-
 156 rations oscillate about their equilibrium positions but
 157 these amplitudes of the vibration are not big enough
 158 to break the bonds between atoms. Therefore, the mater-
 159 ials are still in a crystal state; ii) Upon heating fur-
 160 ther, there is a sudden jump in the total energy per
 161 atom to a higher energy region. This behaviour of the
 162 total energy shows the phase transition often referred
 163 to as a first-order phase transition which is character-
 164 ized by a sudden and discontinuous change in total
 165 energy per atom.

166 Related to Configuration 8 in Table 1, the behavior
 167 of the total energy per atom does not follow any rule
 168 maybe due to the strong effect of the edge size on the
 169 melting process of the configuration leading to the fi-
 170 nite size effects.

171 One can see that the initial configurations are in a
 172 crystal state. When these initial configurations are
 173 heated, the temperature in these configurations in-
 174 creases until these configurations reach their melting
 175 point. At the melting point, these configurations start
 176 to absorb heat energy to undergo the phase transition
 177 into a liquid state while the temperature remains con-
 178 stant until the entire crystal structure has melted. Af-
 179 ter that, the temperature in these configurations in-
 180 creases again. So, the change of the heat with respect
 181 to the temperature (the heat capacity) shows a peak at
 182 the melting point (the phase transition temperature).
 183 In general, the heat capacity is defined as below:

$$C = \frac{\Delta E}{\Delta T} \quad (2)$$

184 In which, E is the total energy per atom, and T is tem-
 185 perature. In this context, the peak of the heat capacity
 186 can be used to define the melting point of the config-
 187 urations.

The heat capacity of eight configurations in Table 1 is
 calculated based on the total energy and is shown in
 Figure 1 (solid line). The melting point of every con-
 figuration is defined at the peak of the heat capacity
 line and presented in Table 2.

Based on the results in Table 2, we can point out the
 following key points:

i) As for Configuration 1 in Table 1 (0.0173770 A/Z
 edge ratio), the melting temperature (5300 K) is
 higher than the other ones (Table 2, Figure 1a). Mean-
 while, regarding Configuration 8 in Table 1 (43.88
 A/Z edge ratio), the phase transition is complicated
 due to the influence of finite size effects (Figure 1h).
 The main reason here is the length of the armchair
 edges between configurations 1 and 8 in Table 1. The
 armchair length in Configuration 1 (0.0173770 A/Z
 edge ratio) is too short compared to the zigzag edge.
 As well known, compared to the zigzag edges, the
 armchair edges contain more dangling bonds which
 are unstable. This results in the armchair edges being
 more susceptible to external factors than the zigzag
 edges. Therefore, in Configuration 1 in Table 1, the
 length of the armchair edge is much shorter than the
 zigzag edge, leading to a high melting temperature in
 the configuration. However, in Configuration 8 in
 Table 1 (43.88 A/Z edge ratio), the A/Z edge ratio is
 43.88, proving that the armchair edge length is nearly
 44 times longer than the zigzag one, leading to finite
 size effects in the melting process. Thus, to have a gen-
 eral view of the influence of armchair and zigzag edge
 lengths, other A/Z ratios are larger than the one of
 Configuration 1 (0.0173770) and smaller than the one
 of Configuration 8 (43.88) (Table 1). This means that
 we need to consider Configurations 2 to 7 in Table 1.

ii) Related to Configurations 2 to 7 in Table 1, the A/Z
 edge ratios range from 0.069510 to 10.745098. Within
 this range of A/Z edge ratio, the melting temperature
 point varies from 3900 to 4300 K (Figure 1, Table 2).
 On average, the melting temperature within this ra-
 tio range is approximately 4180 K. It can be observed

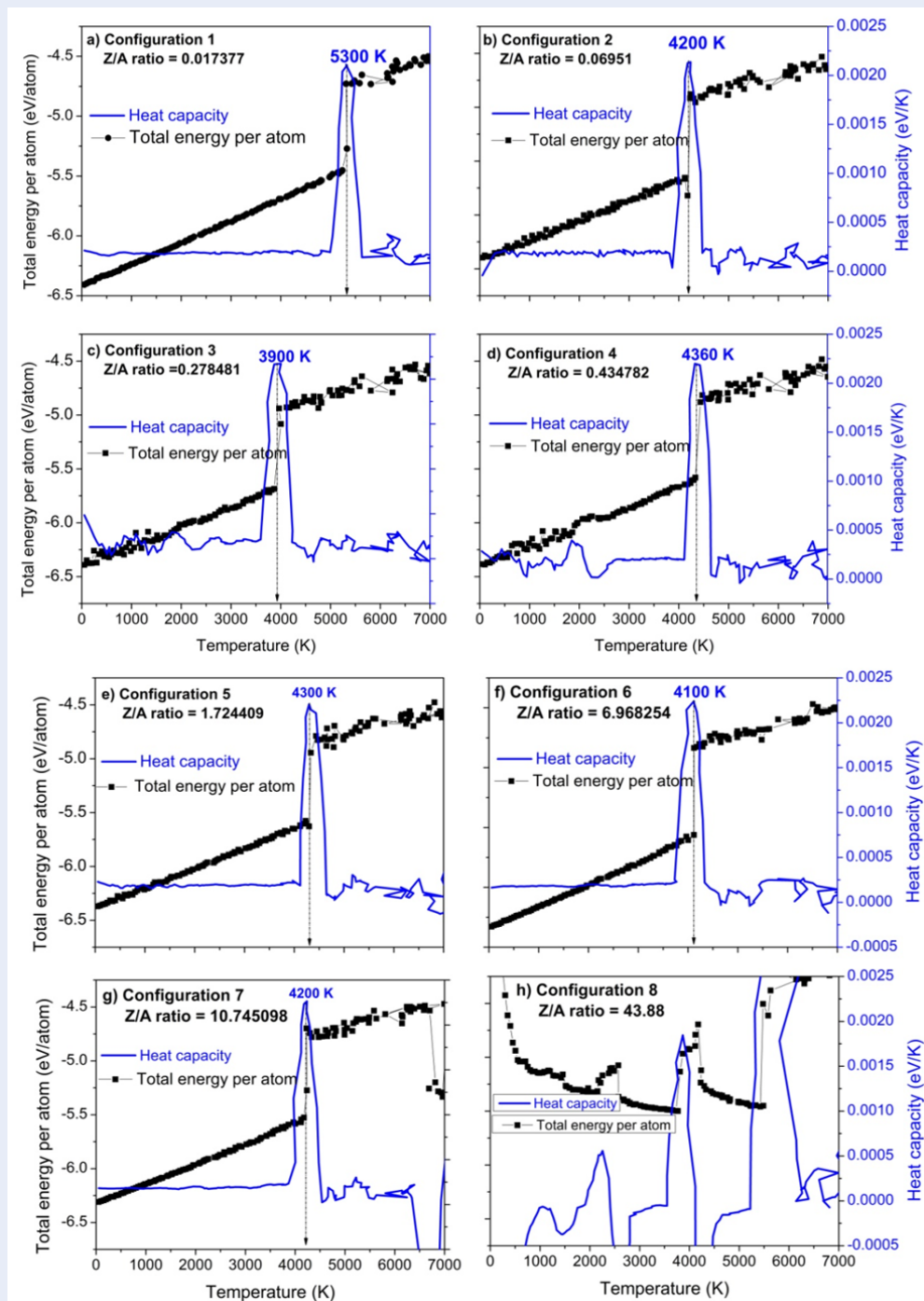


Figure 1: Total energy per atom (square symbol) and heat capacity (solid line) of armchair h-BNNR configurations containing 10,000 atoms in Table 1: a) Configuration 1: A/Z ratio is 0.017377, b) Configuration 2: A/Z ratio is 0.069510, c) Configuration 3: A/Z ratio is 0.278481, d) Configuration 4: A/Z ratio is 0.434782, e) Configuration 5: A/Z ratio is 1.724409, f) Configuration 6: A/Z ratio is 6.968254, and g) Configuration 7: A/Z ratio is 10.745098, h) Configuration 8: A/Z ratio is 43.88.

Table 2: The melting point of different A/Z edge ratios of armchair h-BNNR configurations containing 10,000 atoms.

Configurations	1	2	3	4	5	6	7	8
A/Z ratio	0.017377	0.069510	0.278481	0.434782	1.724409	6.968254	10.745098	43.88
Melting point (K)	5300	4200	3900	4360	4300	4100	4200	..

228 that the A/Z edge ratio does not significantly affect
 229 the melting temperature within this range. Specifi-
 230 cally, Configuration 2 (0.06951 A/Z edge ratio) and
 231 Configuration 7 (10.745098 A/Z edge ratio) in Table 1
 232 both exhibit a melting temperature of 4200 K (Ta-
 233 ble 2). However, the total energy per atom of Con-
 234 figuration 7 is higher than Configuration 2 (Figure 2).
 235 This may be because the Configuration 7 has a longer
 236 armchair edge length than Configuration 2, leading to
 237 the total energy per atom being higher (Tables 1 and
 238 2, Figure 2). Thus, the melting temperature point of
 239 these two configurations (2 and 7) only differs very
 240 slightly from the average temperature point of the left
 241 six configurations in Table 1 (from 2 to 7): 4200 K
 242 versus 4180 K. Therefore, it is necessary to investigate
 243 these two A/Z edge ratios to find a critical A/Z edge
 244 ratio. Note that, the melting point of the configuration
 245 having this critical A/Z edge ratio will not be affected
 246 much when the number of atoms in the configuration
 247 is increased.

253 that all of these configurations exhibit first-type phase
 254 transition (Figure 3). The phase transition temper-
 255 atures of the 10,000, 14,400, 19,600, and 25,600 -
 256 atom configurations are 4200, 3730, 3630, and 3520
 257 K, respectively. One can see that although the differ-
 258 ence in the number of atoms between configura-
 259 tions is about 5000 atoms, there is only a big differ-
 260 ence in the phase transition temperature point of
 261 the 10,000-atom configuration (4200 K) compared to
 262 the 14,400, 19,600, and 25,600 -atom configurations
 263 (3730, 3630, and 3520 K, respectively). The phase
 264 transition temperature points of the left three confi-
 265 gurations (14,400, 19,600, and 25,600 atoms) do not
 266 fluctuate much even though the gap in the number
 267 of atoms between configurations is also 5000 atoms.
 268 Therefore, within the scope of this study, it can be con-
 269 cluded that the phase transition temperature point of
 270 the configurations having 0.06951 A/Z ratio is just rel-
 271 atively stable when the number of atoms in the confi-
 272 guration is from 14,400 to 25,600.

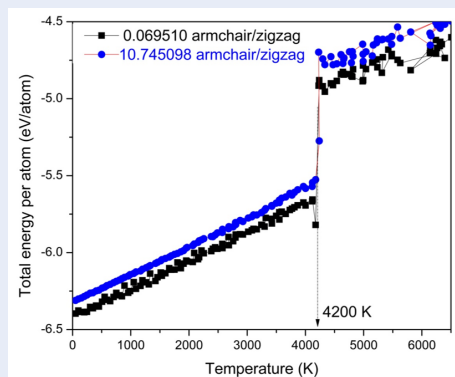


Figure 2: Total energy per atom of armchair h-BNNR configurations containing 10,000 atoms: Configuration 2 in Table 1 (0.069510 A/Z edge ratio) – square symbols and Configuration 7 in Table 1 (10.745098 A/Z edge ratio) – circle symbols.

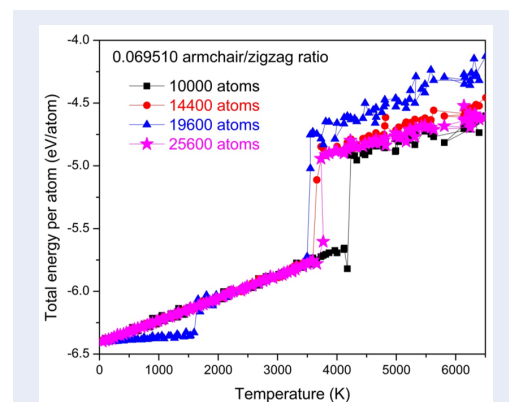


Figure 3: Total energy per atom of armchair h-BNNR configurations with 0.06951 A/Z ratio: 10,000 atoms – square symbols, 14,400 atoms – circle symbols, 19,600 atoms – triangle symbols, and 25,600 atoms – star symbols.

248 First, for Configuration 2 in Table 1 (A/Z ratio of
 249 0.06951), the number of atoms in the configuration
 250 is increased from 10,000 atoms to 14,400, 19,600, and
 251 25,600 atoms, but the A/Z ratio remains the same. Re-
 252 sults from the graph of total energy per atom show

273 As for Configuration 7 in Table 1 (10.745098 A/Z ra-
 274 tio), the number of atoms in the configuration also
 275 increases from 10,000 atoms to 14,400, 19,600, and
 276 25,600 atoms but the A/Z ratio remains the same

(10.745098). The melting temperature points of the 10,000, 14,400, 19,600, and 25,600-atom configurations are 4200, 3940, 4040, and 4040 K, respectively (Figure 4). This means that the melting temperature point of the 10.745098 A/Z case is not affected much by the number of atoms in the configuration even in case of 10,000 atoms (Figure 4). In particular, the melting temperature points of 19,600 and 25,600 - atom configurations are the same as shown in Figure 4 (4040 K). It can be concluded that in the case of the 10.745098 A/Z ratio, the number of 10,000 atoms in the configuration has relatively ensured the stability of the phase transition temperature point. In addition, the noise of total energy in the 10.745098 A/Z configuration is less perturbed than the case of 0.06951 A/Z one (Figures 3 and 4). The reason may be due to the armchair edge length in the case of 10.745098 A/Z ratio being large (Table 1).

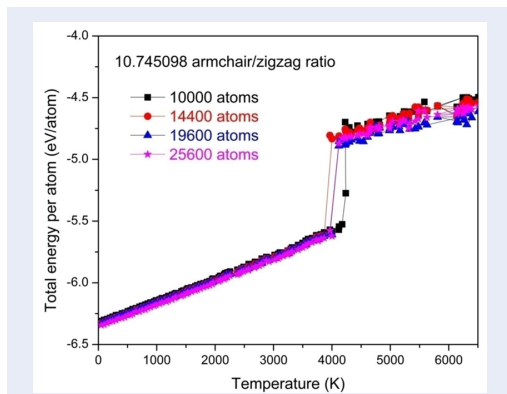


Figure 4: Total energy per atom of armchair h-BNNR configurations with 10.745098 A/Z ratio: 10,000 atoms – square symbols, 14,400 atoms – circle symbols, 19,600 atoms – triangle symbols, and 25,600 atoms – star symbols.

Thus, within the scope of this study, in the case of the 10.745098 A/Z ratio, the configuration containing 10,000 atoms is large enough to ensure the relative stability of the phase transition temperature zone. Therefore, the 10.745098 A/Z ratio can be considered the critical A/Z edge ratio. The 10.745098 A/Z configuration can be visually observed before the melting temperature point (Figure 5a) and at the melting temperature point (Figure 5b).

In addition to Configuration 8 in Table 1 (43.88 A/Z ratio), several visualizations at different temperatures are shown to easily visualize the finite size effects. Based on the peaks in the heat capacity graph (solid line in Figure 1h), several temperature values are chosen and presented in Figure 6. One can see that

the crystal structures in this configuration break at a much lower temperature than those in the remaining configurations in Table 1 due to the finite size effects (Figure 6).

CONCLUSION

The melting process of armchair h-BNNR configuration containing 10,000 atoms is performed with different A/Z ratios to study the dependence of the melting process on the length of the armchair edges and to find the critical A/Z ratio. The Tersoff potential is applied to the interactions between B and N.

- To consider the dependence on A/Z ratios, eight different A/Z ratio configurations (0.017377, 0.069510, 0.278481, 0.434782, 1.724409, 6.968254, 10.745098, and 43.88) of armchair h-BNNR configuration containing the same number of atoms (10,000 atoms) are studied. The results show that the melting process is strongly affected by the configurations with 0.017377 and 43.88 A/Z ratios. The former has a melting point of 5300 K while the latter is affected by the finite size effects. Related to the other configurations, the average value of melting point is 4180 K. And two of them (0.069510 and 10.745098 A/Z ratios) are chosen to find the critical A/Z ratio because these two configurations have the same value of melting point (4200 K) which is closed to the average melting point (4180 K). Note that, the melting point of the configuration with this critical A/Z edge ratio will not be affected much when the number of atoms in the configuration is increased.

- To find the critical A/Z ratio, the A/Z ratios of the two chosen configurations are fixed but the number of atoms in the configuration is increased from 10,000 to 14,400, 19,600, and 25,600 atoms for both 0.069510 and 10.745098 A/Z cases. The results show that the 10.745098 A/Z ratio can be considered the critical A/Z edge ratio because its melting point is not affected much when the number of atoms is increased. In addition, the total energy of the 10.745098 A/Z ratio is less noisy than the one of 0.069510 cases because long the length of the armchair edges.

- The found critical A/Z ratio in this study can be the benchmark for further experimental and theoretical studies.

ABBREVIATIONS

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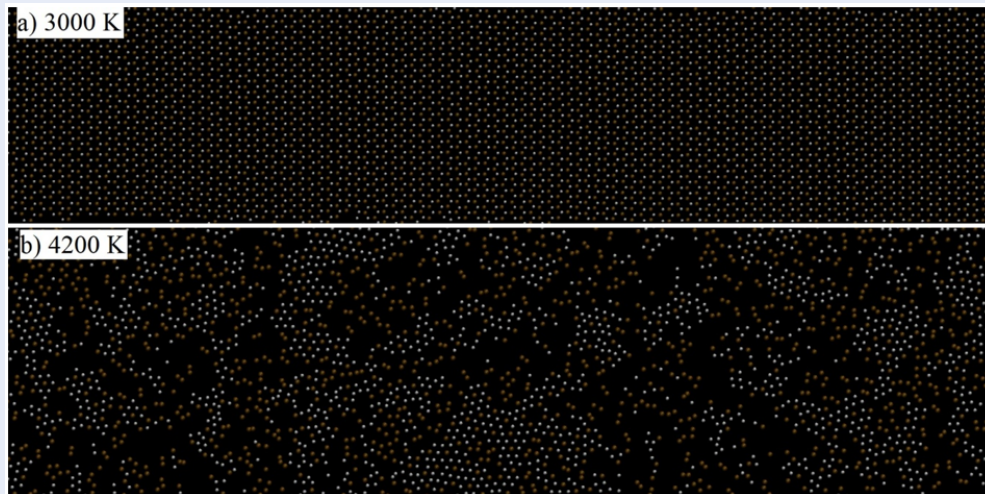


Figure 5: Three-dimensional view of armchair h-BNNR configuration having 10.745098 A/Z ratio at different values of temperature: a) 3000 K, b) 4200 K.

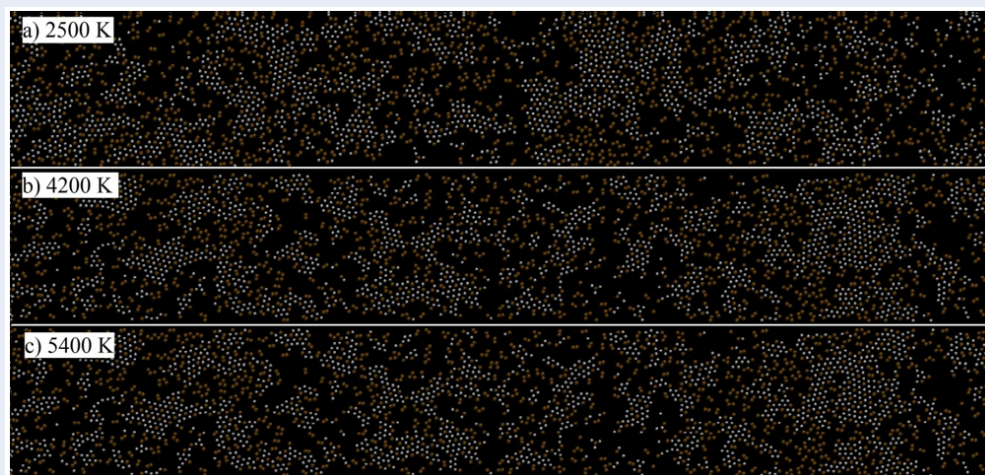


Figure 6: Three-dimensional view of armchair h-BNNR configuration having 43.88 A/Z ratio at different values of temperature: a) 2500 K, b) 4200 K, and c) 5400 K.

359 **AUTHOR'S CONTRIBUTIONS**

360 **FUNDING**

361 **AVAILABILITY OF DATA AND**
362 **MATERIALS**

363 Data and materials used and/or analyzed during the
364 current study are available from the corresponding
365 author on reasonable request.

366 **ETHICS APPROVAL AND CONSENT**
367 **TO PARTICIPATE**

368 Not applicable.

CONSENT FOR PUBLICATION

Not applicable.

COMPETING INTERESTS

The authors declare that they have no competing in-
terests.

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