A comparison of the drying processes used to prepare bacterial cellulose for wound dressing applications

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ABSTRACT

Bacterial cellulose (BC) is a promising polymer because of its ability to manage wound exudation and create a moist environment for healing. The natural form of the BC hydrogel prevents it from maintaining its shape; therefore, water needs to be removed. However, the drying conditions and processing steps can affect the physical characteristics of BC films. This article investigated the effects of drying methods on BC films, revealing structural changes in the membrane. Four different methods are selected, along with methodical research on how drying affects physiological, morphological, and structural properties. As a result, the cold-drying procedure is appropriate for the preparation of BC films for use as wound dressings.

Key words: Bacterial cellulose, cold drying method, wound dressing

INTRODUCTION

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2 Wound management is an essential aspect of health-3 care, and advances in wound dressing materials 4 have contributed to improving healing processes. A 5 promising material for wound dressings is bacterial 6 cellulose, as it possesses unique properties such as bio-7 compatibility, high porosity, and excellent water ab-8 sorption capacity. To fully exploit the potential of 9 bacterial cellulose for wound dressing applications, it 10 is crucial to carefully consider the drying process used during its preparation. This is because the drying pro-12 cess can significantly affect the structure, mechani-13 cal properties, and functionality of bacterial cellulose. 14 Furthermore, different drying methods can lead to 15 variations in the final product, affecting its effective-16 ness in wound healing. Variations in BC membrane characteristics that change under various drying techniques may influence the mechanical characteristics and chemical properties of BC, thus influencing the 20 type of application. The most common straightforward technique for de-22 hydration is the oven drying method (ODM). However, the initial porous microstructure of the raw BC changed throughout these processes. The ODM membrane has a high crystallinity of more than 70%, and the SEM images show that the cellulose fibers are ²⁷ clear and oriented ¹. Another drying method is freeze

28 drying (FDM), which maintains the shape of the fiber

In our study, we investigated the mechanical, chemi-

31 cal, and microstructural properties of BC membranes

due to the decreased surface tension².

by comparing four distinct drying techniques to analyze the notable structural changes in BC. The cold drying method (CDM) involves cooling air in a drying cell below the freezing point on a cold surface, allowing the cold surface to retain moisture, and using 36 dehydrated air for drying³. According to this theory, the morphology of BC is expected to undergo a minor change, and the structure is expected to be preserved. The application at hand, as mentioned above, determines the drying process used. When dried at room 41 temperature, BC films show less crystallinity and little to no change in fiber diameter 4. Therefore, the roomtemperature drying method (RTDM) was used to collate the other drying methods as the control group. The final properties of the materials can be significantly influenced by selecting the appropriate drying technique, so it is possible to adjust the water adsorption capacity, fiber entanglement, or the amount of 49 accessible hydroxyl groups. Therefore, the characteristics of BC films that were dried using various techniques (room temperature, freeze drying, cold drying, and oven drying) are necessary.

MATERIALS AND METHODS

MATERIALS

Fermented bacterial cellulose from *Komagataeibacter xylinus* was purchased from Minh Tam Co., Ltd., Vietnam. Sodium hydroxide (NaOH) (98%) was purchased from Xilong Scientific Co., Ltd., China. All compounds were used as they were without any additional changes.

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62 METHODS

PURIFICATION OF BACTERIAL CELLULOSE

(BC)

65 The raw BC membranes obtained from the Minh Tam Company were washed with DW three times to remove contamination and then soaked in 1 L of DW. Subsequently, the membrane was heated to 100°C for 2 hours and stirred with a magnetic stirrer. The BC membrane was cooled and immersed in 1 M NaOH for 24 h. The acetic acid was removed from the mem-72 brane, and the membrane was continuously washed with DW until it reached pH 7. The purified BC film was finally rinsed with DW, stored in a bag containing DW, and stored in a refrigerator at 4°C.

PREPARATION OF THE DRIED BC MEMBRANE

77 There were four drying methods that followed after 78 the purification process: ODM using drying and heating chambers—Binder ED115, Berlin, Germany—at $60 \pm 1^{\circ}$ C for 16 h; FDM using a vacuum freeze dryer-Labconco 7752020 series, US and Canada-at $42\pm2^{\circ}$ C with pressure at 0.12 mBar for 24 h; RTDM with UV light applied to both sides of BC for 1 h before drying at $26 \pm 2^{\circ}$ C for 144 h; and CDM using AnessicCatore cold dryer- model NWT-35, Italy, at $35 \pm 2^{\circ}$ C for 18 h with a dehydration temperature of 87 -10°C and an air flow rate of approximately 4.0 m/s.

SECOND SERVICE SERVICES

The thicknesses of the purified BC films (4 cm \times 4 cm) were measured before and after the drying process using an analytical balance, and the thickness was measured using an electronic digital caliper. For each sample, three repetitions of each measurement were performed to guarantee repeatability. The BC water content was calculated using the follow-96 ing equation: (1)

Water loss (%) = $\frac{\text{wet weight} - \text{dry weight}}{\text{continuous of the second of the$

98 SURFACE MORPHOLOGY

 99 The BC samples (1 imes 1 cm 2) were observed under a scanning electron microscope (SEM, JSM-IT100, 101 JEOL, Japan) with an acceleration voltage of 10 kV. The BC samples were gold sputter coated prior to analysis.

wet weight

CHEMICAL ANALYSIS

105 Fourier transform infrared spectroscopy was used to analyze the functional groups of the BC samples. (FTIR, Spectrum GX, PerkinElmer Inc., USA) in the wavenumber range of $4000-400 \text{ cm}^{-1}$.

STRUCTURAL CHARACTERISTICS

Using X-ray diffraction (XRD, D8 Advance, Brucker) 110 with Cu Kα radiation, XRD patterns were obtained in 111 the range of $2\theta = 10-80^{\circ}$ with 0.02° steps and 0.5 s per 112 step. The XRD deconvolution method, which separates the crystalline and amorphous contributions to 114 the diffraction spectrum, can be used to calculate the 115 crystallinity of BC.

The ratio of the integrated area under the XRD peaks 117 to the integrated area of all the crystalline peaks can 118 be used to determine the percentage of crystallinity of 119 the samples using Origin Pro 2022.

The percentage crystallinity of BC was calculated using the following equation: (2):

% Crystallinity = $I_c/(I_c+I_a) * 100 (2)$

where the integrated intensities for the amorphous 124 and crystalline phases are denoted by Ia and Ic, respectively.

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MECHANICAL PROPERTIES

The dried BC samples were cut into 1x5 cm² pieces, 128 and an electronic caliper was used to record the thicknesses. A texture analyzer was used to measure the 130 mechanical strength (TA. XT plus, Stable Micro Sys- 131 tems, USA). Three samples in total, each with a maximum load of 1.0 N, were subjected to tests at a strain 133 speed of 0.5 mm/min for each group.

STATISTICAL ANALYSIS

Microsoft Excel was used to perform the statistical 136 analysis, and Origin Pro 2022 was used to graph the 137 data. One-way analysis of variance (ANOVA) was 138 performed, and p < 0.05 was used to determine sig- 139 nificant differences between methods. Student's t test 140 was used for pairwise comparisons of normally distributed data, and p < 0.05 indicated a significant dif-142 ference. Three samples were used for the tests.

RESULTS

Table 1 displays representative physical properties of 145 BC before and after drying. Using Equation (1), the 146 calculation shows that more than 90% of the water 147 is removed during the drying process and causes the 148 water to evaporate, which brings the nanofibers closer 149 together and reduces the thickness of the cellulose pel- 150 licles. Compared to the CDM samples, the FDM and 151 RTDM samples have thicknesses of 0.14 cm, 0.12 cm, 152 and 0.12 cm, respectively, and the ODM sample has a 153 thickness of 0.08 cm. A comparison of the SEM imag- 154 ing data in Figure 1C reveals that the nanofibers of the 155 ODM membranes are braided together to form dis- 156 ordered bundles and that the structure is not porous 157 158 or hollow. Compared to those of membranes dried 159 at room temperature, the fibers bind together to pro-160 duce an indistinguishable array of individual cellulose 161 fibers (Figure 1D). The drying membrane granula-162 tion surface produced by the CDM (Figure 1A) shows 163 intricately connected cellulose fibers packed in large 164 bundles. Cellulose fibers are interwoven and create a 165 compact surface. Figure 1B shows that the lyophilized 166 cellulose membrane has a relatively flat surface.

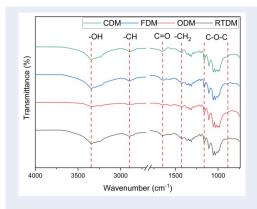


Figure 2: The Fourier-transform infrared (FTIR) spectroscopy results reveal the unique effects of four distinct drying techniques on BC. These techniques are: (A) the Cold-drying method (CDM), (B) the Freeze-drying method (FDM); (C) the Oven-drying method (ODM); and (D) the Room Temperature Drying Method (RTDM). Examination of the FTIR spectra allows for the identification of variations in the functional groups within the structure of BC, corresponding to each drying method used

Table 2: Crystallinity of the dried bacterial cellulose membranes.

Sample	Crystallinity (%)
CDM	59.95
ODM	81.49
FDM	59.09
RTDM	69.56

CDM: Cold-drying method, ODM: Ovendrying method, FDM: Freeze-drying method, RTMD room temperature drying method.

167 However, the density of cellulose fibers produced by
168 the CDM and ODM methods (Figure 1 (A, C)) re169 duces the number of holes between the fibers, and
170 the thickening creates particle bundles on the sur171 face. However, compared to the other samples, the
172 fiber distribution is better organized, resulting in a
173 more porous and hard bulk. A comparison of the
174 BC sample dried at room temperature (RTDM) with

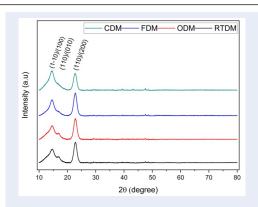


Figure 3: The X-ray diffraction (XRD) patterns yield insights into the influence of four different drying methods on the structure of BC. These methods are: (A) the Cold-drying method (CDM); (B) the Freeze-drying method (FDM); (C) the Oven-drying method (ODM); and (D) the Room Temperature Drying Method (RTDM). Analysis of the XRD patterns reveals variations in the crystallographic features of the BC, each associated with a specific drying method.

that dried using FDM revealed that the former still
maintained its hollow structure and that the latter increased the space between the fibers. Compared with
RTDM, the FDM and CDM techniques are expected
to have desirable fluid absorption capacities and preserve membrane porosity.

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The FTIR spectra of the four drying methods, shown 181 in Figure 2, show BC bands for stretching at approx- 182 imately 3300-3400 cm⁻¹, -CH stretching at approximately 2893 cm⁻¹, and absorbed water at approximately $1649 \text{ cm}^{-1.5}$. The intensity of those peaks for $_{185}$ three samples (CDM, FDM, and RTDM) indicates an 186 increase in the number of -OH groups. It is assumed 187 that there is no water vapor from the atmosphere that 188 is transferred to BC and that, according to experimental studies, the process that transforms bound water 190 into free water is reversible, but the process that transforms free water into evaporated water is irreversible. 192 As stated in a study by Ana R. Rebelo et al., the main 193 method of water loss is the evaporation of free water 6. 194 The free water molecules that reside on the surface of 195 the membrane are the first to evaporate. The hydrogen 196 bond between water and the BC membrane breaks at 197 the same time because of the elevated temperature, 198 releasing water molecules. The volume of water that 199 evaporates increases as free water flows through the 200 BC surface. Air saturation allows free water that has 201 not evaporated to re-evaporate and become bound 202 water, even though the binding constant rate is ex- 203 tremely low⁶. The hydroxyl groups of the bound water could trap the holes in the valence band. Adsorbed 205

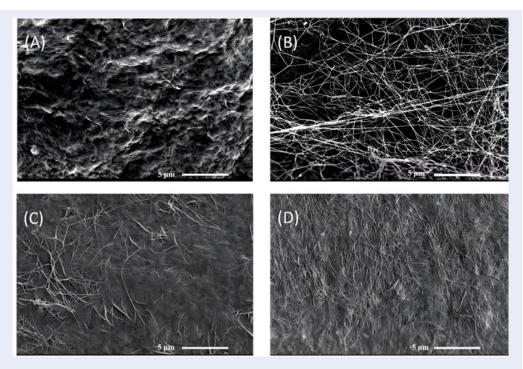


Figure 1: Scanning electron microscope (SEM) images provide visual representations of the surface morphology for four different methods: (A) CDM (Cold-drying method), (B) FDM (Freeze-drying method), ODM (Oven-drying method) and (D) RTDM (room temperature drying method). These images allow us to observe and compare the unique features and structures of BC in each method at the microscale level.

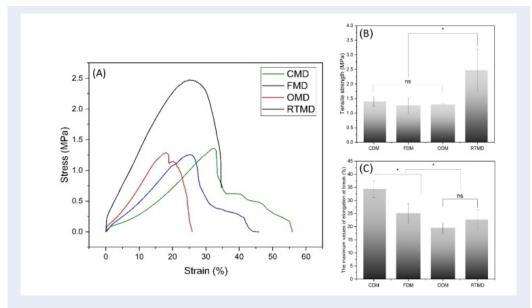


Figure 4: (A) The stress–strain curves, (B) tensile strength, and (C) maximum elongation atbreak (%) of BC films obtained using four different drying methods. * indicates a significant difference (P<0.05), whereas "ns" indicates no significant difference (P>0.05).

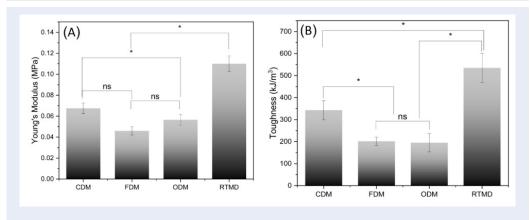


Figure 5: (A) Young's modulus and (B) toughness of BC films were obtained using four different drying methods. * indicates a significant difference (P<0.05), whereas "ns" indicates no significant difference (P>0.05).

Table 1: Physical properties (weight, thickness, water loss)

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SAMPLE	WEIGHT	THICKNESS	WATER LOSS (%)				
Wet (g)	Dry (g)	Wet (cm)	Dry (cm)				
CDM	69.0 ± 6.7	64.7 ± 7.7	14.9 ± 2.1	0.14 ± 0.01	$94\pm8^{\star}$		
FDM	60.8 ± 7.3	49.8 ± 7.9	15.3 ± 0.9	0.12 ± 0.03	$96\pm2^{\star}$		
ODM	67.8 ± 8.8	57.3 ± 8.5	15.3 ± 0.4	0.08 ± 0.01	$94\pm2^{\star}$		
RTDM	62.6 ± 9.4	48.7 ± 5.4	14.6 ± 0.9	0.12 ± 0.03	$91\pm2^*$		

^{*} Means ± SDs indicate significant difference (P<0.05). CDM: Cold-drying method, ODM: Oven-drying method, FDM: Freeze-drying method, RTMD room temperature drying method.

water molecules or surface hydroxyl groups generate OH• radicals. The amount of water loss (%) in the FDM samples during the drying process was greater than that in the CDM, ODM, and RTDM samples. The reason for the differences between the intensity of the absorbed water peaks and the amount of water loss is that the high-temperature drying mechanisms allow water molecules to be easily removed and are unlikely to be converted into bound water. The dehydrated air process of the cold-drying system limited moisture in the water molecules released from the air. An increase in air flow caused more moisture to evaporate from the BC surface, which in turn caused the moisture to move from the BC center to the surface. Peaks corresponding to -CH2 bending vibrations, -CH bending vibrations, OH in-plane bending, and COP stretching appear at wavenumbers of approximately 1431, 1367, 1334, and 1055 cm⁻¹, respectively. Asymmetric and symmetric asymmetric stretching (C-O-C) are present at 1163 cm⁻¹ and 895 cm⁻¹, respectively. The four drying methods (FDM, CDM, ODM, and RTDM) did not change the chemical struc-228 ture of BC during the drying process.

The XRD patterns of the four drying techniques are 229 shown in Figure 3. Three crystalline peaks at 14°, 16°, 230 and 23° are attributed to the (1-10), (110), and (200) 231 crystalline plates, respectively. Using Equation (2), 232 the percentage of crystallinity was calculated. Accord- 233 ing to the XRD calculations, Table 2 shows that ODM 234 has a higher crystallinity than the other methods. The 235 heat energy produced during the oven drying process 236 improved the organization of the amorphous cellulose 237 area, leading to a sample with a crystallinity higher 238 than that of the other samples. Raw BC provided 239 cellulose fibrils with a crystallinity percentage greater 240 than 60%, which is generally found in plant cellulose 4. 241 The degree of crystallinity of BC dried at room tem- 242 perature (RTDM) in this study was 69.56%. When the 243 RTDM samples were compared with the CDM and 244 FDM samples, the former showed a 59.95% decrease 245 in crystallinity, and the latter showed a 59.09% de- 246 crease. Defect structures (porosity), such as cavities 247 and nooks, reduced the degree of crystallinity in the 248 CDM and FDM samples. The cavity and layer struc- 249 ture were the reasons for the reduced crystallinity of 250 BC^{7} .

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The tensile strength and elongation under maximum stress were used to compare the mechanical characteristics of the four drying techniques, as shown in Figure 4. The RTDM had a tensile strength and elongation at a maximum stress of 2.47 \pm 0.71 MPa and $22.67 \pm 3.69\%$, respectively. Compared to the FDM and CDM samples, the RTDM samples exhibited a greater tensile strength. The higher crystallinity and dense fibrous network in the RTDM samples are the cause of this difference. Although the ODM samples have the highest percentage of crystallinity, an increase in temperature during the drying process can cause thermal degradation of BC, breakage of chemical bonds, and loss of structural integrity, resulting in the samples having the lowest tensile strength. CDM films have greater elongation at maximum stress than do ODM, RTDM, and FDM films. CDM BC exhibited the typical behavior of resilient materials with high elongation under maximum stress and very little strain before fracture. The CDM prevented the loss of water because moisture was retained by

stress than do ODM, RTDM, and FDM films. CDM
BC exhibited the typical behavior of resilient materials with high elongation under maximum stress and
very little strain before fracture. The CDM prevented
the loss of water because moisture was retained by
the cold surface and thus prevented the nanocellulose
fibers from breaking. The mechanism is the flow of air
used in the drying process 8. Consequently, compared
to ODM and FDM, the films were demonstrated to
elongate more prior to breaking. The tensile strengths
of the RTDM film are also significantly greater than
those of the three drying methods.

Compared to ODM, realignment may be limited by lower porosity and higher order (high crystallinity), resulting in lower tensile strength and strain. In contrast, an increase in tensile strength and deformation (Figure 4) in RTDM can be caused by strain hardening of the nanofibrous membrane caused by unraveling of the cellulose chains in the amorphous area and realignment of the fibers in the loading direction.

The calculation of Young's modulus, which is sometimes referred to as the modulus of elasticity, involves dividing the longitudinal stress by the strain. FDM BC showed less ductile behavior, with a low Young's modulus (Figure 5A) and a considerable maximum elongation at break before fracture (Figure 4). The tensile strength varies very little, although FDM exhibits low tensile strain, which may be related to larger pores (100–250 nm) being deformed compared to those of the other samples (Figure 1B).

Figure 5B shows that the toughness of the CDM and RTDM samples was greater than that of the ODM and FDM samples. The toughness was mathematically expressed as U = E/V, where V is the volume, U is the toughness, and E is the total energy from the start to fracture. It is also connected to the region under the stress-strain curve that extends from the rupture

point to the start of the deformation. The RTDM sample $(535\pm65~{\rm kJ/m^3})$ has a greater toughness than the CDM sample $(343\pm43~{\rm kJ/m^3})$, which means that the RTDM sample can be resilient. One of the characteristics of wound dressings is toughness, or the ability to withstand plastic deformation without breaking. Better wound protection is made possible by the structure in which wound dressings are formed during the drying process and are maintained without breaking under stress.

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DISCUSSION

Research on BC characteristics, including surface 316 morphology and physical-chemical properties, re- 317 vealed that the drying techniques used had a signif- 318 icant impact. BC is naturally produced as a thin layer 319 of hydrogel with more than 90% water content in its 320 microfiber network⁹. This reveals the high porosity 321 and capacity of the material to store water. However, 322 the amount of water in the BC membrane needs to be 323 partially removed to make it more suitable for making a membrane for gauze applications. ODMs are 325 commonly used for water removal. However, dur- 326 ing these processes, the original microporous structure of the material in the water-absorbing state significantly changes (Figure 1C) 10. Freeze drying is another membrane drying technique that helps to main- 330 tain the shape and porosity of fibers by preventing coagulation of microfibrils/microcrystals (Figure 1B) 11. 332 In this approach, the water in BC first freezes and then 333 decreases to be evacuated as vapor.

The relationships between the surface morphology, 335 XRD data, and mechanical characteristics explain the 336 trends observed for each drying method. The SEM 337 image of the well-organized RTDM fibers (Figure 1D) 338 demonstrates their exceptional mechanical charac- 339 teristics. However, compared to other procedures, 340 the RTDM approach yields a smaller amount of wa- 341 ter that is eliminated, which requires a longer drying 342 time and ideal sterilization conditions. Compared to 343 those of the other two techniques, the SEM results 344 show that CDM and FDM enable the preservation of 345 the porous structure of BC. CDM, FDM, and RTDM 346 preserve bound water molecules, while ODM com- 347 pletely removes free water molecules, disrupts hydro- 348 gen bonds, and reduces the number of surface OH 349 groups. It follows that ODM is appropriate for pre- 350 serving BC membranes. Unlike ODM, which has 351 the highest crystallinity, ODM has the lowest elonga- 352 tion at break (19.56%), followed by RTDM and FDM 353 (22.6% and 25.1%, respectively). CDM showed the 354 highest elongation at break, approximately 34.38%, 355 with high Young's modulus and toughness values of 356 $_{357}$ 0.06 \pm 0.004 MPa and 343 \pm 43 kJ/m 3,respectively . 358 It should be mentioned that because the appropriate 359 tensile strength range for a wound dressing is 1 to 32 360 MPa, which is determined by the thickness of the hu-361 man skin layer and satisfies the predetermined physi-362 cal requirements at a largely adequate level, the deformation capacity must be greater than 30% ¹².

CONCLUSIONS

From the results of the analysis, CDM BC was determined to be suitable for the production of wound dressing membranes because this method can remove more than 94% of the water while retaining optimal properties compared to other methods. In addition to maintaining the chemical structure of BC, BC has low crystallinity (59%) and ideal mechanical properties, with a tensile strength of 1.4 MPa and a maximum elongation at break of 34.3%, which is suitable for making wound dressings.

LIIST OF ABBREVIATIONS USED

BC: Bacterial cellulose

377 SEM: Scanning electron microscopy

378 XRD: X-ray diffraction

379 FTIR: Fourier transform infrared

380 CDM: Cold-drying method

ODM: Oven-drying method

382 FDM: Freeze-drying method

383 RTDM: Room-temperature drying method

COMPETITIVE INTERESTS

The authors declare that they have no conflicts of interest.

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AUTHORS' CONTRIBUTION

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